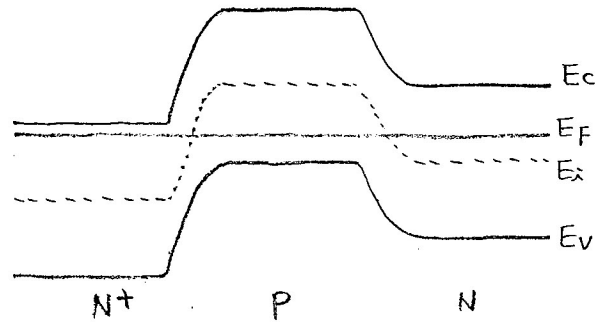


HW#5 SOLUTION

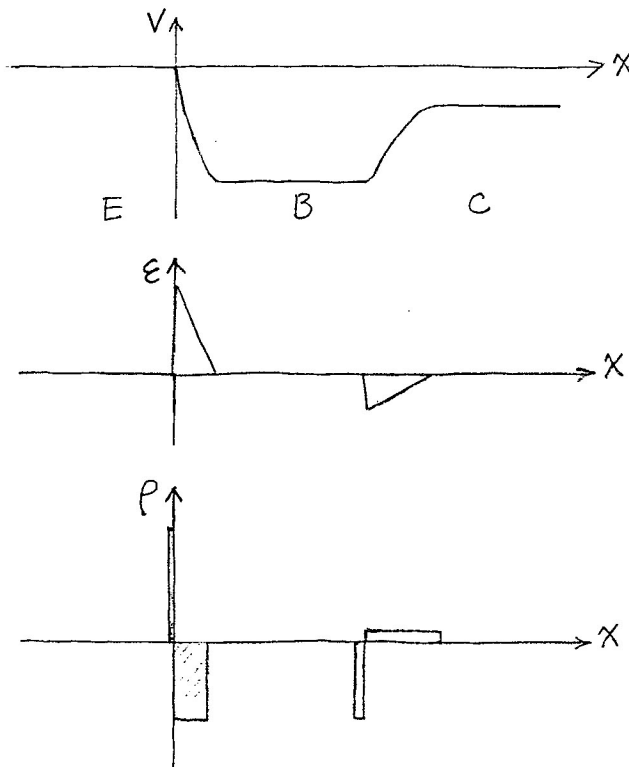
1) prob. 10.4.

a) For the given doping concentrations, one computes $E_F - E_i = 0.477 \text{ eV}$, -0.358 eV , and 0.298 eV respectively in the emitter, base, and collector.

Also, with $N_{DE} \gg N_{AB}$, the E-B depletion width will lie almost exclusively in the base. Likewise, the majority of the C-B depletion width will lie in the collector. The diagram produced by BJT_Eband program is displayed below.



b)



$$\begin{aligned}
 c) \quad \Delta V_{CE} &= \frac{1}{q} [(E_F - E_i)_{\text{collector}} - (E_F - E_i)_{\text{emitter}}] \\
 &= \frac{KT}{q} [\ln(N_{DC}/n_i) - \ln(N_{DE}/n_i)] \\
 &= \frac{KT}{q} \ln(N_{DC}/N_{DE}) = -0.179 \text{ V}
 \end{aligned}$$

d) Analogous to Eq 10.3 in the text,

$$W = W_B - X_{PEB} - X_{PCB}$$

$$\text{Where, } X_{PEB} \approx \left[\frac{2K_s \epsilon_0}{q N_{AB}} V_{biEB} \right]^{1/2} = 3.30 \times 10^{-5} \text{ cm}$$

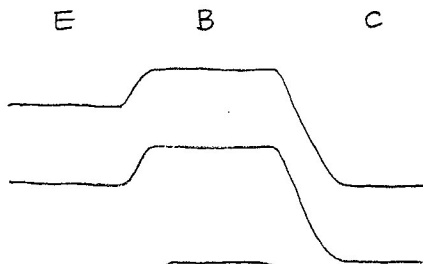
$$X_{PCB} = \left[\frac{2K_s \epsilon_0}{q N_{AB}} \cdot \frac{N_{DC}}{N_{DC} + N_{AB}} \cdot V_{biCB} \right]^{1/2} = 8.82 \times 10^{-6} \text{ cm}$$

$$\therefore W = 2 \times 10^{-4} - 3.30 \times 10^{-5} - 8.82 \times 10^{-6} = 1.58 \times 10^{-4} \text{ cm.}$$

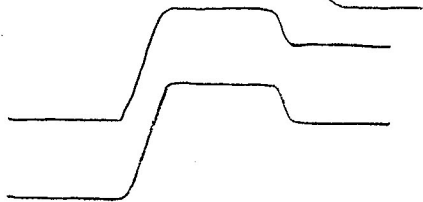
$$e) \quad E_{\text{max}(E-B)} = \frac{q N_{AB}}{K_s \epsilon_0} X_{PEB} = 5.06 \times 10^4 \text{ V/cm}$$

$$|E|_{\text{max}(C-B)} = \frac{q N_{AB}}{K_s \epsilon_0} X_{PCB} = 1.35 \times 10^4 \text{ V/cm}$$

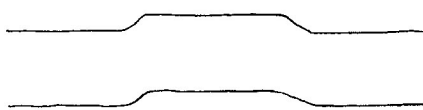
α) i) active bias mode:



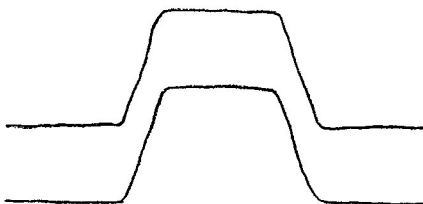
ii) inverted bias mode:



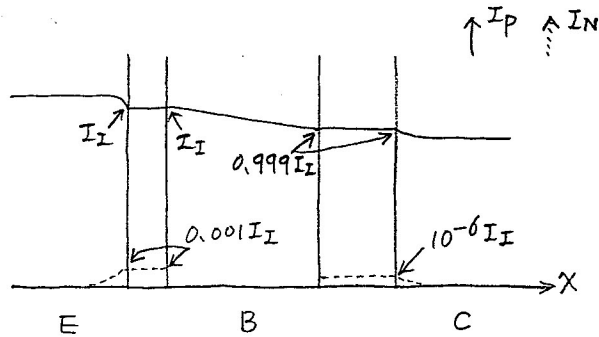
iii) saturation mode:



iv) cut off mode:



2) prob. 11.2



$$a) \gamma = \frac{I_{EP}}{I_{EP} + I_{EN}} = \frac{I_I}{1.001 I_I} = 0.9990$$

$$b) \alpha_T = \frac{I_{CP}}{I_{EP}} = \frac{0.999 I_I}{I_I} = 0.9990$$

$$c) \alpha_{dc} = \gamma \alpha_T = 0.9980$$

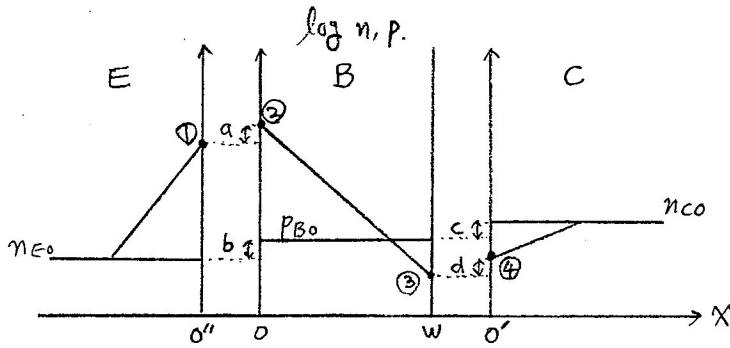
$$\beta_{dc} = \frac{\alpha_{dc}}{1 - \alpha_{dc}} = 499$$

d) method 1. $I_E = I_{EP} + I_{EN} = 1.001 I_I$
 $I_C = I_{CP} + I_{CN} = 0.999 I_I + 10^{-6} I_I$
 $I_B = I_E - I_C = 1.999 \times 10^{-3} I_I$

method 2. $I_{B1} = I_{EN} = 0.001 I_I$
 $I_{B2} = I_{EP} - I_{CN} = 0.001 I_I$
 $I_{B3} = -I_{CN} = -(10^{-6}) I_I$
 $I_B = I_{B1} + I_{B2} + I_{B3} = 1.999 \times 10^{-3} I_I$

e) Yes. All currents on the figure are constant across the depletion regions. This implies (see subsection 6.1.2) that recombination-generation is negligible in these regions.

3) i) point A is in active region.



for point ① $\Delta n_E(o'') = n_{E0} (e^{\frac{qV_{EB}}{kT}} - 1)$

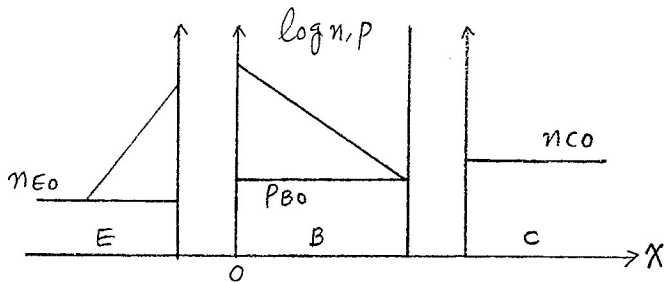
" ② $\Delta P_B(o) = P_{B0} (e^{\frac{qV_{EB}}{kT}} - 1)$

" ③ $\Delta P_B(w) = P_{B0} (e^{\frac{qV_{CB}}{kT}} - 1)$

" ④ $\Delta n_C(o') = n_{C0} (e^{\frac{qV_{CB}}{kT}} - 1)$

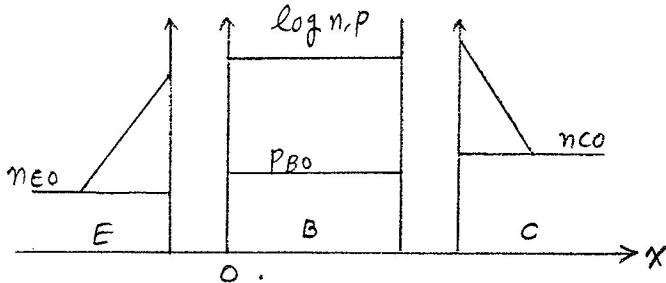
\therefore we see $a=b, c=d$.

ii) point B is in onset saturation region.



$\cdot V_{CB}$ have zero value.
So, $n_C(x) = n_{C0}$.

iii) point C is in strong saturation region.



$\cdot I_C = q A D_B \frac{dP_B(x)}{dx}$ have to be zero.
So, $P_B(x)$ is constant.

4)

a) From eq. 10.3

$$W = W_B - X_{PEB} - X_{PCB}$$

$$\text{where, } N_{DE} = 10^{18} \text{ cm}^{-3}, N_{AB} = 10^{16} \text{ cm}^{-3}, N_{DC} = 10^{15} \text{ cm}^{-3}$$

$$W_B = 1.0 \times 10^{-4} \text{ cm}$$

$$(E_F - E_i)_E = KT \ln \frac{N_{DE}}{n_i} = 0.477 \text{ eV}$$

$$(E_F - E_i)_B = -KT \ln \frac{N_{AB}}{n_i} = -0.358 \text{ eV}$$

$$(E_F - E_i)_C = KT \ln \frac{N_{DC}}{n_i} = 0.298 \text{ eV}$$

$$\left. \begin{array}{l} \\ \\ \end{array} \right\} \Rightarrow \begin{array}{l} V_{biEB} = 0.835 \text{ V} \\ V_{biCB} = 0.656 \text{ V} \end{array}$$

$$X_{PEB} \approx \left(\frac{2K_s \epsilon_0}{q N_{AB}} V_{biEB} \right)^{1/2} = 3.30 \times 10^{-5} \text{ cm}$$

$$X_{PCB} = \left(\frac{2K_s \epsilon_0}{q N_{AB}} \frac{N_{DC}}{N_{DC} + N_{AB}} V_{biCB} \right)^{1/2} = 8.82 \times 10^{-6} \text{ cm}$$

$$\therefore W = 1 \times 10^{-4} - 0.33 \times 10^{-4} - 0.0882 \times 10^{-4} = 0.58 \times 10^{-4} \text{ cm}$$

b) Since $e^{qV_{EB}/KT} \gg 1$ and $e^{qV_{CB}/KT} \ll 1$, we can write the following: (NPN)

$$I_{En} = q n_i^2 A \cdot \frac{D_B}{W N_B} \cdot e^{qV_{EB}/KT}$$

$$I_{Ep} = q n_i^2 A \cdot \frac{D_E}{L_E N_E} \cdot e^{qV_{EB}/KT}$$

$$I_{Cn} = q n_i^2 A \cdot \left(\frac{D_B}{W N_B} - \frac{W}{2 \tau_B \cdot N_B} \right) \cdot e^{qV_{EB}/KT}$$

$$I_{Cp} = q n_i^2 A \cdot \left(\frac{D_C}{L_C N_C} \right)$$

$$\text{where, } D_B = 0.026 \times 1248 = 32.45$$

$$D_E = 0.026 \times 115 = 2.99$$

$$D_C = 0.026 \times 458 = 11.91$$

$$L_E = \sqrt{D_E \tau_E} = 1.7 \times 10^{-3} \text{ cm}, \text{ assume } \tau_E = \tau_C = \tau_B = 1 \mu\text{s}$$

$$L_C = \sqrt{D_C \tau_C} = 3.45 \times 10^{-3} \text{ cm}$$

$$A = 0.01 \text{ cm}^2$$

$$W = 1 \times 10^{-4} - 2.55 \times 10^{-5} - 2.44 \times 10^{-5} = 5.01 \times 10^{-5} \text{ cm}$$

$$\therefore I_{En} = 2.3298 \times 10^{-3} \text{ (A)}$$

$$I_{Ep} = 6.32 \times 10^{-8} \text{ (A)}$$

$$I_{Cn} = 2.3296 \times 10^{-3} \text{ (A)}$$

$$I_{Cp} = 5.52 \times 10^{-11} \text{ (A)}$$

c) Including Base recombination,

$$I_B = I_{B\text{ideal}} + I_{B\text{recomb.}}$$

$$= q n_i^2 A \left(\frac{D_E}{L_E N_E} + \frac{W}{2\tau_B} \cdot \frac{1}{N_B} \right) (e^{qV_{EB}/kT} - 1) \\ + q n_i^2 A \left(\frac{D_C}{L_C N_C} + \frac{W}{2\tau_B} \cdot \frac{1}{N_B} \right) (e^{qV_{CB}/kT} - 1)$$

$$I_C = I_{C\text{ideal}} - I_{B\text{recomb}} \approx I_{C\text{ideal}}$$

$$I_E = I_{E\text{ideal}}$$

$$\gamma (\text{emitter injection efficiency}) = \frac{I_{EP}}{I_{EP} + I_{EN}} = 0.99997$$

$$\alpha_T (\text{base transport factor}) = \frac{I_{CP}}{I_{EP}} = 0.99991$$

$$\alpha_{dc} = \gamma \cdot \alpha_T = 0.99988$$

$$\beta_{dc} = \frac{\alpha_{dc}}{1 - \alpha_{dc}} = 8.33 \times 10^3$$

d) for reducing the length of emitter to $0.3 \mu\text{m}$,

I_{EP} is same, but

I_{EN} is increase because.

$$I_{EN} = q n_i^2 A \cdot \frac{D_E}{L_E N_E} e^{qV_{EB}/kT}, \quad W_E \ll L_E, \text{ so} \\ L_E \text{ have to be replaced by } W_E.$$

So, $I_{EN} \uparrow \Rightarrow \gamma \downarrow \Rightarrow \beta \downarrow$.

It would increase I_{EN} and decrease β .

5)

$$a) I_C = q n_i^2 A \left(\frac{D_B}{W N_B} \right) \left(e^{2V_{EB}/KT} - 1 \right) - q n_i^2 A \left(\frac{D_C}{L_C N_C} + \frac{D_B}{W N_B} \right) \left(e^{2V_{CB}} - 1 \right)$$

$$\text{where } e^{2V_{EB}} \gg 1, e^{2V_{CB}} \ll 1$$

$$\approx q n_i^2 A \cdot \frac{D_B}{W \cdot N_B} \cdot e^{2V_{EB}/KT}$$

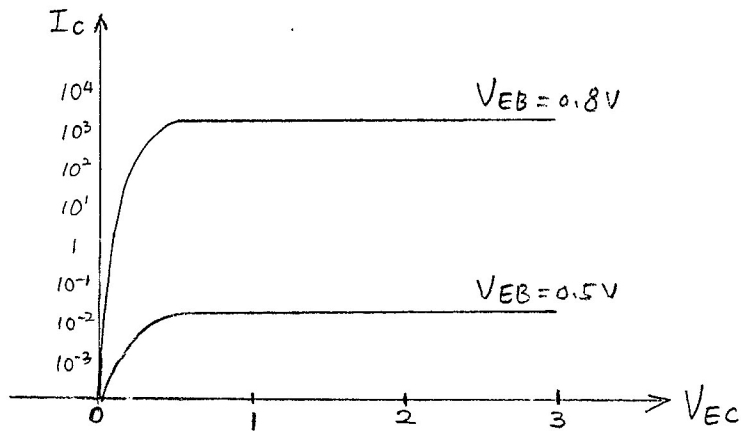
$$\text{where, } D_B = 0.026 \times 378 = 9.83 \text{ cm}^2 \text{ s}^{-1}$$

∴ when $V_{EB} = 0.5 \text{ V}$,

$$I_C = 2.3 \times 10^{-2} \text{ (A)}$$

when $V_{EB} = 0.8 \text{ V}$,

$$I_C = 2.2 \times 10^3 \text{ (A)}$$



$$b) I_B = q n_i^2 A \left(\frac{D_E}{L_E N_E} + \frac{W}{2\tau_B} \cdot \frac{1}{N_B} \right) \cdot e^{2V_{EB}/KT} \text{ for active region,}$$

$$\text{where } A = 1 \text{ cm}^2$$

$$D_E = 0.026 \times 300 = 7.8$$

$$L_E = \sqrt{D_E \tau_E} = 0.88 \times 10^{-3} \text{ cm.}$$

$$\tau_B = 5 \times 10^{-7}$$

$$W = 0.32 \times 10^{-4} \text{ cm.}$$

$$N_B = 5 \times 10^{16} \text{ cm}^{-3}$$

$$N_E = 8 \times 10^{17} \text{ cm}^{-3}$$

$$\therefore \text{ when } V_{EB} = 0.5 \text{ V, } I_B = 4.22 \times 10^{-7} \text{ (A)}$$

$$\text{when } V_{EB} = 0.8 \text{ V, } I_B = 4.32 \times 10^{-2} \text{ (A)}$$

c) From eq. 11.49,

$$I_C \approx q n_i^2 A \frac{D_B}{W \cdot N_B} e^{2V_{EB}/KT}$$

Where $D_B = 9.83$

$V_{EB} = 0.8$

$N_B = 5 \times 10^{16}$

$W = 0.6 \times 10^{-4} - X_{nEB} - X_{nCB}$

$$= 0.6 \times 10^{-4} - \left(\frac{2K_s \epsilon_0}{q \cdot N_{DB}} \cdot \frac{N_{AE}}{N_{AE} + N_{DB}} \cdot V_{EB} \right)^{1/2} - \left(\frac{2K_s \cdot \epsilon_0}{q \cdot N_{DB}} \cdot \frac{N_{AC}}{N_{AC} + N_{DB}} (V_{b_{iCB}} - V_{CB}) \right)^{1/2}$$

$$= 0.56 \times 10^{-4} - 1.6 \times 10^{-5} \times (0.76 - V_{CB})^{1/2}$$

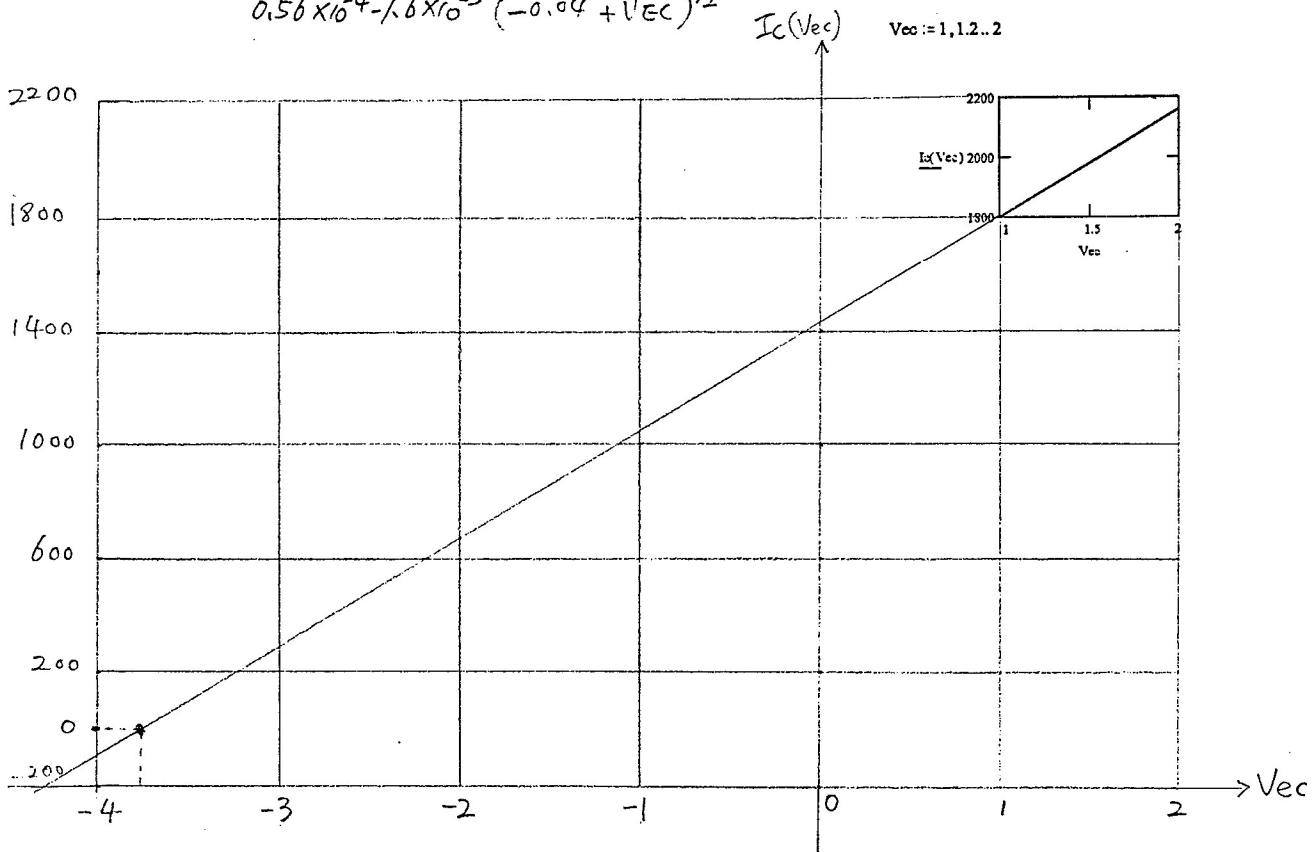
where $V_{CB} = V_{EB} - V_{EC} = 0.8 - V_{EC}$

$$I_C = 16 \times \frac{9.83}{5 \times 10^{16}} \times e^{30.77} \times \frac{1}{0.56 \times 10^{-4} - 1.6 \times 10^{-5} \times (-0.04 + V_{EC})^{1/2}}$$

$$= \frac{7.26 \times 10^{-2}}{0.56 \times 10^{-4} - 1.6 \times 10^{-5} \times (-0.04 + V_{EC})^{1/2}}$$

$$I_C(V_{EC}) := \frac{7.26 \cdot 10^{-2}}{.56 \cdot 10^{-4} - 1.6 \cdot 10^{-5} \cdot \sqrt{-.04 + V_{EC}}}$$

$V_{EC} := 1, 1.2 \dots 2$



∴ Early Voltage ≈ -3.8 V

d)

$$W = W_B - X_{nEB} - X_{nCB}$$

$$= 0.6 \times 10^{-4} - \left[\frac{2K_s \epsilon_0}{q} \frac{N_E}{N_B(N_E + N_B)} (V_{biEB} - V_{EB}) \right]^{1/2} - \left[\frac{2K_s \epsilon_0}{q} \frac{N_C}{N_B(N_C + N_B)} (V_{biCB} - V_{CB}) \right]^{1/2}$$

$$\text{where } V_{biEB} = 0.026 \ln \frac{N_E N_B}{n_i^2} = 0.874$$

$$V_{biCB} = 0.026 \ln \frac{N_C N_B}{n_i^2} = 0.76$$

$$V_{EB} = 0.5 \text{ V}$$

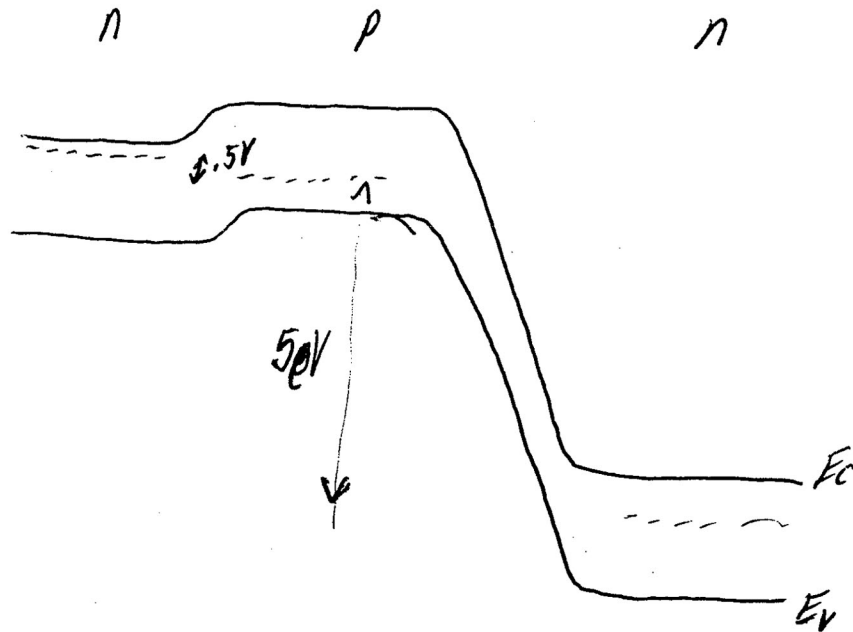
$$W = 0.6 \times 10^{-4} - 0.96 \times 10^{-5} - \left[0.43 \times 10^{-10} (0.76 - V_{CB}) \right]^{1/2}$$

the condition for punch through is $W=0$, so,

$$0 = 5.04 \times 10^{-5} - 0.65 \times 10^{-5} \sqrt{0.76 - V_{CB}}$$

$$\therefore V_{CB} = -59.36 \text{ (V)}$$

6. a) Forward Active Bias



Emitter $N_d = 10^{17}$ or 10^{16}

$$E_c - E_f = -kT \ln \frac{N_d}{N_c} = .21 \text{ eV for } N_d = 10^{16}$$

$$= .15 \text{ eV " } N_d = 10^{17}$$

Base $N_a = 10^{15} \text{ cm}^{-3}$

$$E_v - E_f = -kT \ln \frac{N_a}{N_v} = .24 \text{ eV}$$

Collector $N_d = 10^{14}$

$$E_c - E_f = -kT \ln \frac{N_d}{N_c} = .33 \text{ eV}$$

b) $I_x \leftrightarrow I_E$ for npn

$I_z \leftrightarrow I_C$

This is forward active so we can assume $e^{qV_x/kT} \gg 1 \gg e^{-qV_z/kT}$

$$I_E = I_X = q n_i^2 A \left(\frac{D_{E1}}{2W_{E1}N_{E1}} + \frac{D_{E2}}{2W_{E2}N_{E2}} + \frac{D_B}{W_B N_B} \right) \times e^{-qV_X/kT}$$

2 mm^2 (under A)
 $\sim 3 \mu\text{m}$ (under W_{E1})

$$I_C = q n_i^2 A \left[\frac{D_B}{W_B N_B} - \left(\frac{W_B}{2L_B} \frac{1}{N_B} \right) \right] e^{-qV_X/kT}$$

$$N_B = 10^{15} \text{ cm}^{-3} A = 2 \text{ mm}^2$$

$$W_B = 3 \mu\text{m} - X_{pE} - X_{pC}$$

$$= 3 \mu\text{m} - \sqrt{\frac{2e}{q} (V_{biE} - 0.5) \frac{N_d}{N_a} \frac{1}{(N_a + N_d)}}$$

$$- \sqrt{\frac{2e}{q} (V_{biC} + 0.5) \frac{N_d}{N_a} \frac{1}{(N_a + N_d)}}$$

$$V_{biE} \approx .65 \text{ V or } .71 \text{ V} \left(\frac{kT}{q} \ln \frac{N_a N_d}{n_i^2} \right)$$

$$V_{biC} \approx .53 \text{ V}$$

$$W_B = 3 \mu\text{m} - .5 \mu\text{m} - .81 \mu\text{m}$$

$$\underline{W_B \approx 1.7 \mu\text{m}}$$

$$D_B = \frac{kT}{q} \mu_{nB} (10^{15}) = (0.026)(1345)$$

$$D_B = 35 \frac{\text{cm}^2}{\text{s}}$$

$$I_Z (= I_C) = q n_i^2 A \left(\frac{D_B}{W_B N_B} - \frac{W}{2W_B N_B} \right) e^{-qV_Z/kT}$$

\downarrow
 very small
 compared to $\frac{D}{W}$

$$I_Z \approx 18 \text{ mA}$$

c1)

$$\gamma = \frac{\frac{D_B}{W_B N_B}}{\frac{D_{E1}}{2W_{E1}N_{E1}} + \frac{D_{E2}}{2W_{E2}N_{E2}} + \frac{D_B}{W_B N_B}}$$

$$\frac{D_B}{W_B N_B} \approx 2.1 \times 10^{-10}$$

$$W_{E1} \sim W_{E2} \sim 3 \mu\text{m}$$

(Note that $x_{nE} < 0.05 \mu\text{m}$)
($< 2\%$ of W_E)

$$D_{E1} = \frac{kT}{q} \mu_p (10^{17}) = (0.026)(391) = 8.6 \frac{\text{cm}^2}{\text{s}}$$

$$D_{E2} = \frac{kT}{q} \mu_p (10^{16}) = (0.026)(437) = 11.4 \frac{\text{cm}^2}{\text{s}}$$

$$\frac{D_{E1}}{2W_{E1}N_{E1}} = 1.4 \times 10^{-13}$$

$$\frac{D_{E2}}{2W_{E2}N_{E2}} = 1.9 \times 10^{-12}$$

$$\gamma = .99$$

$$\alpha_T = 1 - \frac{W_B^2}{2L_B^2}$$

$$L_B = \sqrt{D_B \tau_B}$$
$$= \sqrt{35 \frac{\text{cm}^2}{\text{s}} (.1 \times 10^{-8} \text{s})}$$

$$L_B \approx 19 \mu\text{m}$$

$$\alpha_T = 1 - \frac{1}{2} \left(\frac{1.2}{19} \right)^2$$

$$\alpha_T = .996$$

$$\beta = \frac{\gamma \alpha_T}{1 - \gamma \alpha_T}$$

$$\beta \approx 71$$

d.)

$$I_{CC} = I_Z = 18 \text{ mA}$$

$$I_{BB} = \frac{18 \text{ mA}}{20} \quad I_{BB} = .9 \text{ mA}$$

$$\tau_r = \tau_B \ln \left[\frac{1}{1 - \left(\frac{18}{.9} \frac{1}{71} \right)} \right]$$

$$\tau_r = .1 \mu\text{s} (.33)$$

$$\tau_r = 33 \text{ ns}$$

$$\tau_B / 4 = \beta$$

could also use
 $\tau_t = \frac{W^2}{2D_B}$

e.)

$$I_c = \frac{M \alpha_{dc}}{1 - M \alpha_{dc}} I_B$$

$$\text{Now } \frac{\alpha_{dc}}{1 - \alpha_{dc}} = 71$$

\therefore Let "significant" mean 10%
(Other reasonable values ok.)

$$\text{Find } \frac{M \alpha_{dc}}{1 - M \alpha_{dc}} \approx 78 \quad \alpha_{dc} = .986$$

$$(M \alpha_{dc}) = 78 - 78/M \alpha_{dc}$$

$$79 M \alpha_{dc} = 78$$

$$M \alpha_{dc} = \frac{78}{79}$$

$$M = 1.001$$

$$M = \frac{1}{1 - \left(\frac{V_{CEQ}}{V_{CBO}}\right)^m} \quad \text{let } m = 6$$

$$V_{CBO} = \frac{\epsilon}{2q} \frac{N_A + N_D}{N_A N_D} \epsilon_{cr}^2$$

$$\underline{V_{CBO} = 5700 \text{ V}}$$

$$1 - \left(\frac{V_{CE}}{V_{CB0}}\right)^6 = \frac{I}{M}$$

$$1 - \frac{I}{M} = \left(\frac{V_{CE}}{V_{CB0}}\right)^6$$

$$V_{CE} = V_{CB0} \left(1 - \frac{I}{M}\right)^{1/6} = 5700 \left(1 - \frac{I}{1.001}\right)^{1/6}$$

$$\underline{V_{CE} \sim V_Z \sim 1800V}$$

Not a significant contribution to base current until this value is reached ($\sim 1800V$) but significant beyond that.