

## Lecture 23

11/30/12

### Linear Systems

#### Controllability

Transfer non-zero initial state to zero

$$x(k+1) = A x(k) + B u(k)$$

$$x(k) = A^k x(0) + R_k \underline{u}_k$$

$$-A^k x(0) = R_k \underline{u}_k$$

Continuous time System :

$$\dot{x}(t) = A x(t) + B u(t)$$

$$x(t) = e^{At} x_0 + \int_0^t e^{A(t-\tau)} B u(\tau) d\tau$$

Note!

Reachability  $\Leftrightarrow$  Controllability

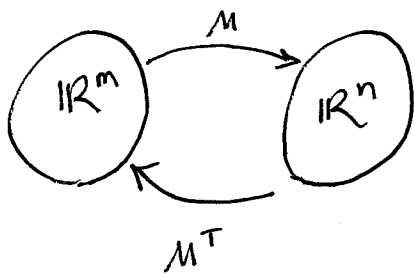
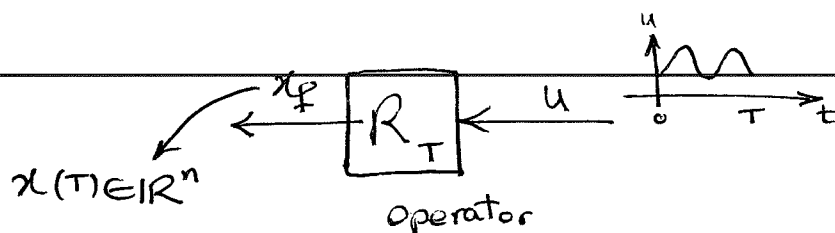
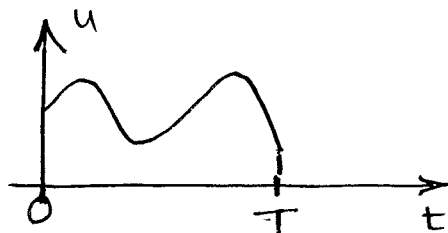
$e^{At}$  : invertible

$x_0 = 0$  and study reachability

$[0, T]$

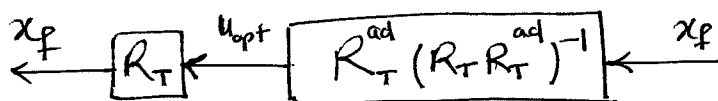
$$x(T) = x_f = \int_0^T e^{A(T-\tau)} B u(\tau) d\tau = [R_T u](T)$$

Control  $u[0, T]$   
 $\hookrightarrow$  function on interval  $[0, T]$



Everything holds for CT from DT by replacing transposes by its adjoint.

Fact: Minimum energy control



$$P_T = \int_0^T e^{At} B B^T e^{A^T t} dt = R_T R_T^{\text{ad}}$$

$$\frac{dP_T}{dT} = AP + PA^T + BB^T$$

Fact 1 : Controllability in CT is not influenced by the choice of  $T$  (final time)

Fact 2 : Kalman rank test holds:

System reachable (controllable)



$$\text{rank}([A^{n-1}B \mid \dots \mid B]) = n$$

Fact 3 : PBH test and Kalman Canonical forms for unreachable systems carry over ~~from~~ from DT.

$$\text{rank}([sI - A \mid B]) = n$$

$$u_{\text{opt}}(t) = \underbrace{B e^{A^T t}}_{R_T^{\text{ad}}} \cdot \underbrace{P_T^{-1}}_{\downarrow} x_f$$

Controllability gramian at time  $T$

## Observability

Determines our ability to estimate states from limited measurements.

$$\text{DT: } \begin{aligned} x(k+1) &= Ax(k) \\ y(k) &= Cx(k) \end{aligned}$$

$A, C$  : model of our system (given matrices)

$y$  : measured output

$x$  : state [we want to estimate]

$$x(k) = A^k \cdot x(0)$$

so your ability to see the state at stage  $k$  depends on your ability to see  $x(0)$  with limited measurements.

Ex M.S. system

$$\begin{aligned} \begin{matrix} \text{position} \swarrow \\ \text{velocity} \swarrow \end{matrix} \begin{bmatrix} P(k+1) \\ V(k+1) \end{bmatrix} &= \begin{bmatrix} * & * \\ * & * \end{bmatrix} \begin{bmatrix} P(k) \\ V(k) \end{bmatrix} \\ y(k) &= \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} P(k) \\ V(k) \end{bmatrix} \end{aligned}$$

Position measurements ✓  
unknown velocity

Key question: can we determine initial condition  
from limited ("potentially" noisy)  
measurements.

$$y(0) = C x(0)$$

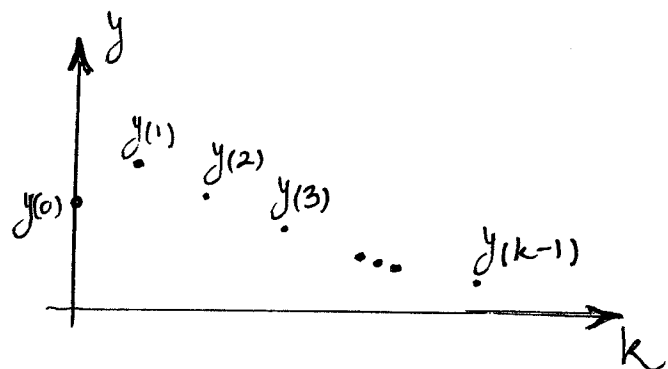
$$y(1) = C x(1) = C A x(0)$$

⋮

$$y(k-1) = C x(k-1) = \dots = C A^{k-1} x(0)$$

$$\underbrace{\begin{bmatrix} y(0) \\ \vdots \\ y(k-1) \end{bmatrix}}_{\text{measured (known)}} = \underbrace{\begin{bmatrix} C \\ CA \\ \vdots \\ CA^{k-1} \end{bmatrix}}_{\text{model ("known")}} \cdot \underbrace{x(0)}_{\text{unknown}}$$

$$\underline{y}_k = O_k x(0)$$



$\text{Null}(O_k)$  : determines initial conditions that cannot be distinguished from zero initial conditions.

\* System  $x(k+1) = Ax(k)$  is observable  
 $y(k) = Cx(k)$

$\Uparrow$  (equivalent to)  
 $\Downarrow$

$$\text{rank}(O_n) = n$$

$n$  : # of states

$$(\text{Null}(O_n) = \{0\})$$

$$O_n = \begin{bmatrix} C \\ CA \\ \vdots \\ CA^{n-1} \end{bmatrix}$$

$$\text{rank}(O_n) = \text{rank}(O_n^T)$$

$$O_n^T = \begin{bmatrix} C^T & A^T C^T & \dots & (A^T)^{n-1} C^T \end{bmatrix}$$

$\downarrow \quad \downarrow \quad \downarrow$   
 $\bar{B} \quad \bar{A} \quad \bar{B}$

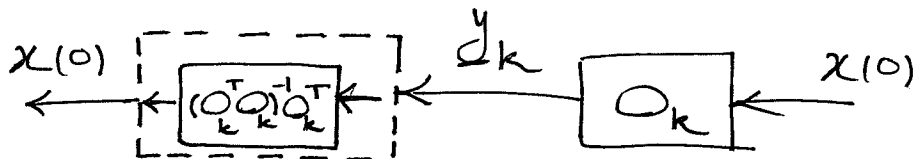
$$= [\bar{B} \mid \bar{A} \bar{B} \mid \dots \mid (\bar{A})^{n-1} \bar{B}] \quad \text{reachability matrix of system:}$$

$$z(k+1) = A^T z(k) + C^T u(k)$$

So observability of the system  $x(k+1) = Ax(k)$   
 $y(k) = Cx(k)$

is equivalent to the reachability of the system

$$x(k+1) = A^T z(k) + C^T u(k)$$



$$y(k) = Cx(k) + \underbrace{w(k)}_{\text{measurement noise}}$$

$$\underline{w}_k = \begin{bmatrix} w(0) \\ \vdots \\ w(k-1) \end{bmatrix}$$

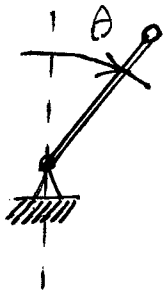
$$\underline{y}_k = O_k x(0) + \underline{w}_k$$

$$\begin{bmatrix} y \\ \underline{y}_k \end{bmatrix} = \begin{bmatrix} O_k \end{bmatrix} \begin{bmatrix} x(0) \end{bmatrix} + \begin{bmatrix} \underline{w}_k \end{bmatrix}$$

skinny matrix

$$(O_k^T O_k) = \sum_{i=0}^{k-1} (A^i)^T C^T C A^i$$

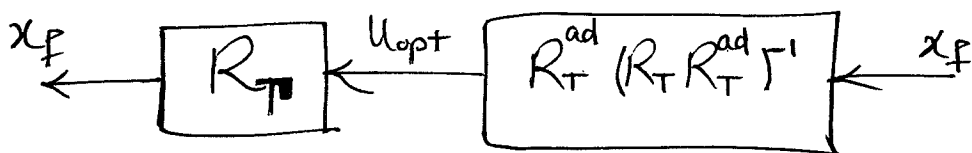
State-feedback design :



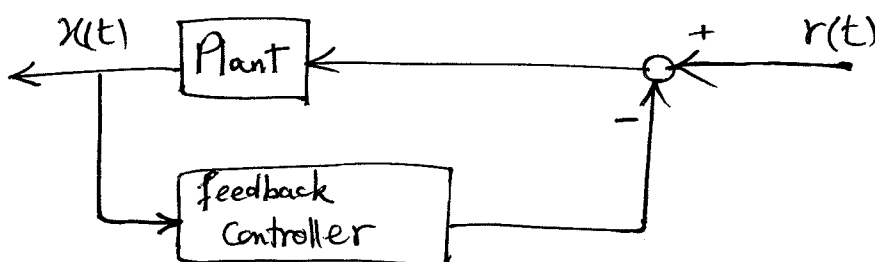
$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u(t)$$

Want to measure  $x_1(t)$  and  $x_2(t)$  and to use these measurements to achieve some objective

$$u(t) = -[k_1 \ k_2] \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + r(t) \quad \text{reference signal}$$



open loop control



$K_1, K_2$  : feedback gains

(#'s that determine how we should process  
our measurements)

↓  
 $x_1(t)$  &  $x_2(t)$

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 1-K_1 & -K_2 \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} r(t)$$

↓

$$f(s) = \det(sI - A_{cl}) = s(s+K_2) - 1 + K_1$$

$$= s^2 + K_2 s + K_1 - 1 = (s - \lambda_1)(s - \lambda_2)$$