

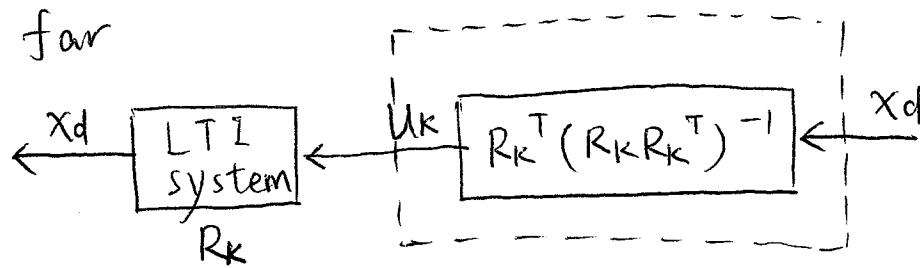
Last time:

- ctrl of cts time systems
- obsv (very briefly)

Today:

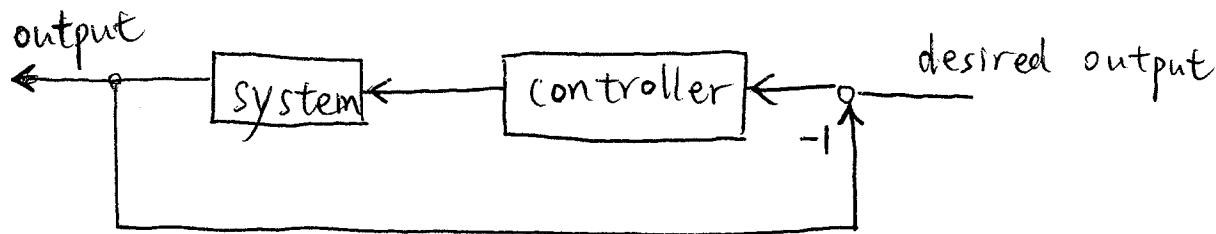
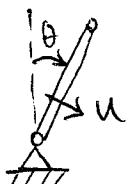
- "Pole placement" (state feedback design)
- Observer (estimator) design
- Output feedback design (Observer based design)

So far



Problem : open-loop strategy
 (doesn't pay attention to measurements)

Alternative : use feedback

State feedback :

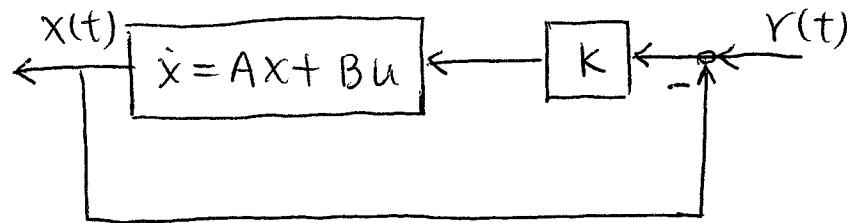
$$\text{state} \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$\dot{x} = Ax + Bu \quad (1)$$

state feedback controller

$$u(t) = -Kx(t)$$



$$u(t) = -Kx(t) + r(t) \quad (2)$$

↓ ↓ ↓
 Control state feedback measured state
 signal matrix K

reference signal

For $r(t) \equiv 0$, plug (2) \rightarrow (1)

$$\Rightarrow \dot{x}(t) = Ax(t) - BKx(t)$$

$$\Rightarrow \dot{x}(t) = \underbrace{(A - BK)}_{Acl} x(t)$$

Want to design K to move eigenvalues of Acl to arbitrary location in the LHP.

Fact: This can be achieved iff system (1) is controllable.

Matlab: `place(A, B, Edes)`

$$I.P. \quad u(t) = -Kx(t)$$

$$= -[K_1 \ K_2] \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix}$$

$$Acl = A - BK = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} - \begin{bmatrix} 0 \\ 1 \end{bmatrix} [K_1 \ K_2]$$

$$Acl = \begin{bmatrix} 0 & 1 \\ 1-k_1 & -k_2 \end{bmatrix}$$

$$\begin{aligned} f_{cl}(s) &= \det(sI - Acl) \\ &= \det \begin{bmatrix} s & -1 \\ k_1-1 & s+k_2 \end{bmatrix} \\ &= s^2 + k_2 s + k_1 - 1 \\ &\stackrel{\text{Want}}{=} (s+\lambda_1)(s+\lambda_2) \\ &= s^2 + (\lambda_1 + \lambda_2)s + \lambda_1\lambda_2 \\ &(= s^2 + 2\zeta\omega_0 s + \omega_0^2) \end{aligned}$$

For stability: $k_1 > 1$
 closed-loop $k_2 > 0$

Observer (Estimator) design

FF Last time

$$\dot{x} = Ax$$

$$y = cx + w(t)$$

$$y(t) = ce^{At}x_0$$

Rather than estimating the initial condition, we'll try to design a dynamical system (estimator/observer) where state should go to the "real state" as $t \rightarrow \infty$.

setup:

original system

$$\begin{aligned}\dot{x} &= Ax + Bu \quad \text{--- (1)} \\ y &= Cx\end{aligned}$$

known input

$x(0)$ = not known

Naive observer:

$$\dot{\hat{x}} = A\hat{x} + Bu \quad \text{--- (2)}$$

$\hat{x}(0)$: under my control

$$\tilde{x}(t) = x(t) - \hat{x}(t)$$

↓ ↓
observation observer
error state

$$(1) - (2)$$

$$\frac{d}{dt}(x - \hat{x}) = A(x - \hat{x}) + Bu - Bu$$

$$\dot{\tilde{x}}(t) = A\tilde{x}(t)$$

$$\tilde{x}(0) \neq 0$$

Want $\hat{x}(t) \xrightarrow{t \rightarrow \infty} x(t)$

\Updownarrow

$$\tilde{x}(t) \xrightarrow{t \rightarrow \infty} 0$$

will hold iff $\text{Re}(\lambda_i(A)) < 0$, for all $i=1, \dots, n$

Fix of the naive observer:

$$\begin{aligned}\dot{\hat{x}} &= A\hat{x} + Bu + \underbrace{L(y(t) - \hat{y}(t))}_{\text{an "injection" term}} \\ \hat{y} &= C\hat{x}(t)\end{aligned}$$

$$\dot{\hat{x}} = A\hat{x} + Bu + L \underbrace{C(x(t) - \hat{x}(t))}_{\tilde{x}(t)} \quad \text{--- (3)}$$

(1) - (3)

$$\dot{\tilde{x}}(t) = A\tilde{x}(t) - LC\tilde{x}(t)$$

Error dynamics:

$$\dot{\tilde{x}}(t) = (A - LC)\tilde{x}(t)$$

Fact: can design matrix L to move e-values of $A - LC$ to arbitrary location in LHP iff (A, C) observable



pair (A^T, C^T) controllable



design \bar{K} , s.t. $\bar{A} - \bar{B}\cdot\bar{K}$ has desired e-values.
where $\bar{A} = A^T$, $\bar{B} = C^T$, $\bar{K} = L^T$.

$$\tilde{x}(t) = x(t) - \hat{x}(t) = e^{(A-LC)t} \tilde{x}(0)$$

I.P. Ex:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

$$y = [1 \ 0] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$A - LC = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} - \begin{bmatrix} l_1 \\ l_2 \end{bmatrix} [1 \ 0] = \begin{bmatrix} -l_1 & 1 \\ 1 - l_2 & 0 \end{bmatrix}$$

Fast convergence of $\hat{x}(t)$ to $x(t)$ requires "large" observer gain L .

Drawback : NOISE

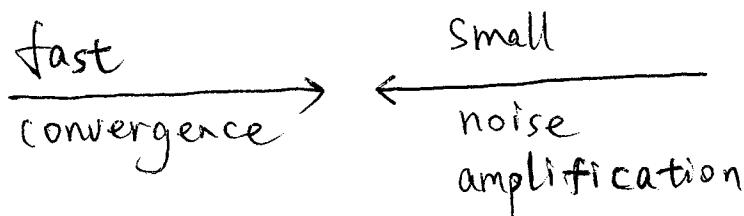
Original system

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + w(t)$$

↳ measurement noise

$$\dot{\tilde{x}}(t) = (A - LC)\tilde{x}(t) + L \cdot w(t)$$



Kalman filter: optimal observer

- Observer-based controller
(optimal feedback design)

state feedback

$$u(t) = -Kx(t)$$

An option:

Use an observer-based controller of the form

$$\dot{\hat{x}} = A\hat{x} + Bu + L(y - \hat{y})$$

$$u = -K\hat{x}$$

$$\dot{x} = Ax - BK\hat{x} \quad \text{--- (a)}$$

$$\dot{\hat{x}} = LCx + (A - BK - LC)\hat{x} \quad \text{--- (b)}$$

$$\begin{bmatrix} \dot{x} \\ \dot{\hat{x}} \end{bmatrix} = \begin{bmatrix} A & -BK \\ LC & A - BK - LC \end{bmatrix} \begin{bmatrix} x \\ \hat{x} \end{bmatrix}$$

K, L design variables

Approach: rewrite.

Pg 90

$$\begin{bmatrix} x \\ \tilde{x} \end{bmatrix} = \begin{bmatrix} I & 0 \\ I & -I \end{bmatrix} \begin{bmatrix} x \\ \hat{x} \end{bmatrix}$$

$$(a) \Rightarrow \dot{x} = Ax - BK(x - \tilde{x}) \\ = (A - BK)x + BK\tilde{x}$$

$$(a) - (b) \Rightarrow \dot{\tilde{x}} = (A - LC)\tilde{x}$$

$$\begin{bmatrix} x \\ \tilde{x} \end{bmatrix} = \begin{bmatrix} A - BK & BK \\ 0 & A - LC \end{bmatrix} \begin{bmatrix} x \\ \tilde{x} \end{bmatrix}$$

If (A, B) controllable,
 (A, C) observable,

can choose K & L s.t. e-values of $Acl @$
arbitrary location