

Lecture 24

Wednesday, April 20, 2011
5:01 PM

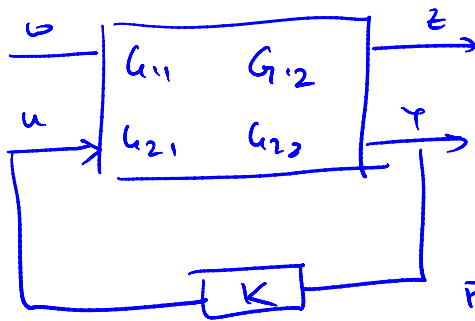


Fig 1 :

⊙ Let $G \equiv \left[\begin{array}{c|cc} A & B_1 & B_2 \\ \hline c_1 & D_{11} & D_{12} \\ c_2 & D_{21} & D_{22} \end{array} \right]$ ✓ can always be assumed is stab. and detectable

⊙ Suppose that the inherited realization of $G_{22} \equiv \left[\begin{array}{c|c} A & B_2 \\ \hline c_2 & D_{22} \end{array} \right]$ is also stabilizable and detectable

⊙ The stability of the $(G-K)$ interconnection in Fig 1 is equivalent to the stability of the feedback interconnection of $(G_{22}-K)$ given by

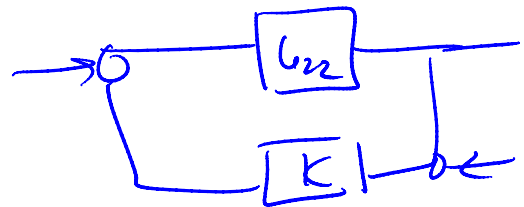


Fig 2

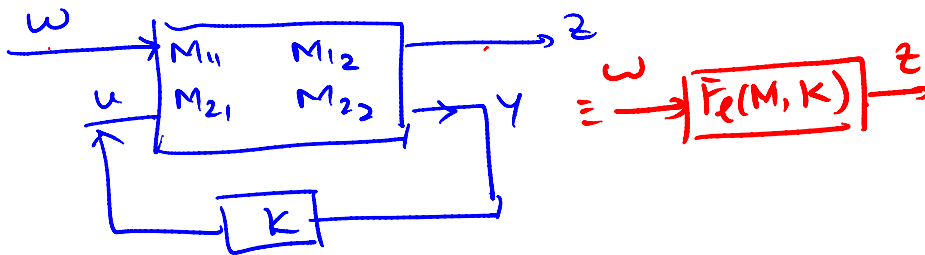
⊙ From Youla parametrization all stabilizing controllers is given by $(Y-M\Theta)(X-N\Theta)^{-1}$

for fig 2: and therefore for Figure 1.

⊙ Assuming that $\left(\begin{array}{c|c} A & B_2 \\ \hline c_2 & D_{22} \end{array} \right) \equiv G_{22}$ is stab. and detectable all ~~are~~ closed-loop

maps in Figure 1 can be written as $H = UQV$ where Q is any stable parameter.

Lower Linear fractional transformation:



$$\begin{bmatrix} z \\ y \end{bmatrix} = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} \begin{bmatrix} w \\ u \end{bmatrix}$$

$$u = Ky$$

$$\begin{cases} z = M_{11}w + M_{12}u \\ y = M_{21}w + M_{22}u \\ u = Ky \end{cases} \Rightarrow \begin{cases} y = M_{21}w + M_{22}Ky \\ \Rightarrow (I - M_{22}K)y = M_{21}w \end{cases}$$

$$\Rightarrow y = (I - M_{22}K)^{-1} M_{21}w$$

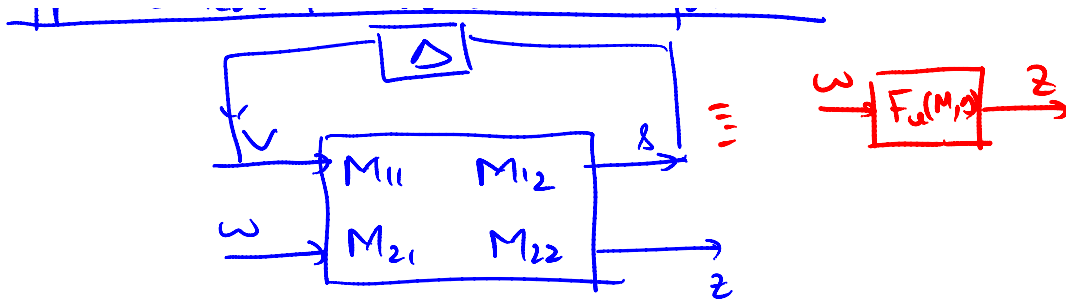
$$\Rightarrow z = M_{11}w + M_{12}K(I - M_{22}K)^{-1} M_{21}w$$

$$\Rightarrow z = \underbrace{\left[M_{11} + M_{12}K(I - M_{22}K)^{-1} M_{21} \right]}_{F_e(M, K)} w$$

$$F_e(M, K)$$

$$z = F_e(M, K) w$$

Upper Linear Fractional Transformation



$$\begin{pmatrix} \delta \\ z \end{pmatrix} = \begin{bmatrix} M_{11} & M_{12} \\ M_{21} & M_{22} \end{bmatrix} \begin{bmatrix} V \\ \omega \end{bmatrix} \quad \left. \begin{array}{l} \delta = M_{11}V + M_{12}\omega \\ z = M_{21}V + M_{22}\omega \end{array} \right\}$$

$$V = \Delta \delta$$

$$\begin{aligned} \delta &= M_{11}V + M_{12}\omega \Rightarrow \delta = M_{11}\Delta\delta + M_{12}\omega \\ &\Rightarrow \delta = (I - M_{11}\Delta)^{-1} M_{12}\omega. \end{aligned}$$

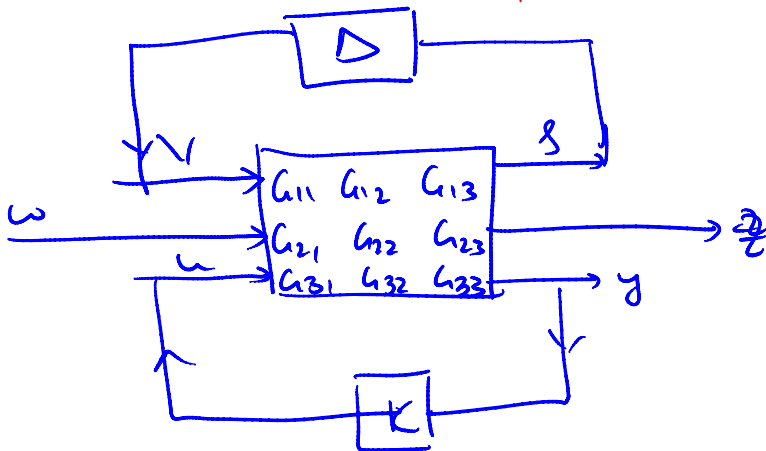
$$z = M_{21}V + M_{22}\omega$$

$$= M_{21}\Delta(I - M_{11}\Delta)^{-1} M_{12}\omega + M_{22}\omega$$

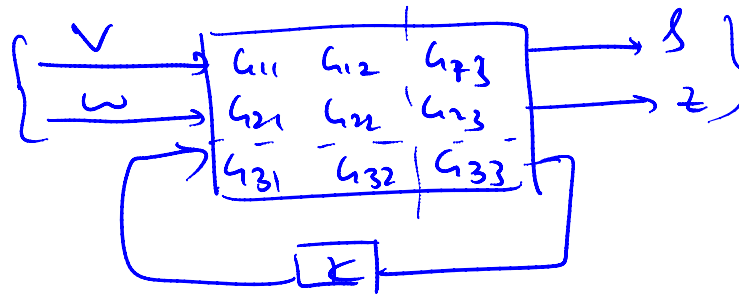
$$= \underbrace{(M_{22} + M_{21}\Delta(I - M_{11}\Delta)^{-1} M_{12})}_{F_u(M, \Delta)} \omega$$

$F_u(M, \Delta)$.

$(G-K-\Delta)$ framework

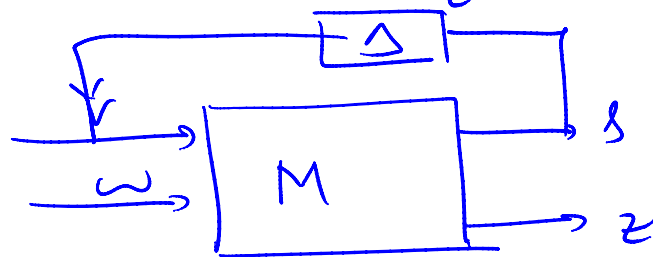


$$\begin{pmatrix} \delta \\ z \\ y \end{pmatrix} = \begin{bmatrix} G_{11} & G_{12} & G_{13} \\ G_{21} & G_{22} & G_{23} \\ G_{31} & G_{32} & G_{33} \end{bmatrix} \begin{bmatrix} V \\ \omega \\ u \end{bmatrix}$$



$\begin{pmatrix} V \\ w \end{pmatrix} \mapsto \begin{pmatrix} y \\ z \end{pmatrix}$ is given by

$$\begin{pmatrix} y \\ z \end{pmatrix} = F_e(G, K) \cdot \begin{bmatrix} V \\ w \end{bmatrix}$$



$$M = F_e(G, K)$$

\therefore the map from w to y is

$$F_u(M, \Delta) = F_u[F_e(G, K), \Delta]$$

\therefore The closed-loop map is given by

$$z = \underbrace{F_u[F_e(G, K), \Delta]}_x w.$$

The following properties of Fractional transformers are

① Suppose C is an invertible matrix then

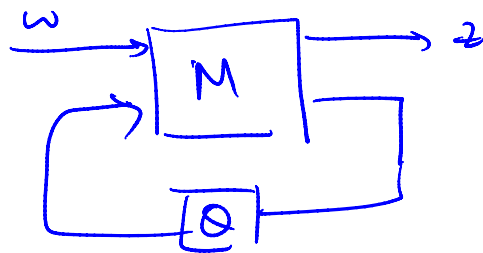
$$\textcircled{2} (A + BQ)(C + DQ)^{-1} = F_e(M, Q)$$

$$\dots (C + DQ)^{-1} (A + BQ)^{-1} = I - (C + DQ)^{-1} BQ$$

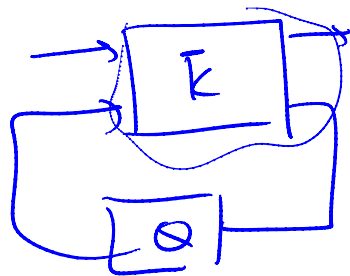
$$\rightarrow (C + D\bar{O})^{-1} (A + D\bar{B})^{-1} \equiv F_u(N, \bar{O})$$

$$\text{where } M \equiv \begin{bmatrix} AC^{-1} & B - AC^{-1}D \\ C^{-1} & -C^{-1}D \end{bmatrix}$$

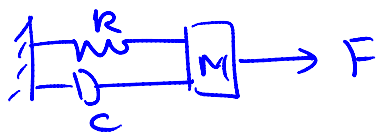
$$N \equiv \begin{bmatrix} C^{-1}A & C^{-1} \\ B - DC^{-1}A & -DC^{-1} \end{bmatrix}$$



$w \mapsto z$ is given
by
 $(A + B\bar{O})(C + D\bar{O})^{-1}$



Parametric Uncertainty: An Example



⊙ The system is a spring-mass-damper system with a force as an input to the mass.

⊙ The dynamics is given by

$$\ddot{x} + \frac{c}{m} \dot{x} + \frac{k}{m} x = \frac{F}{m}$$

⊙ Let say that the parameters of the

model; k, m and c are all uncertain;
 suppose they are uncertain by 10%. Thus,
 the following hold

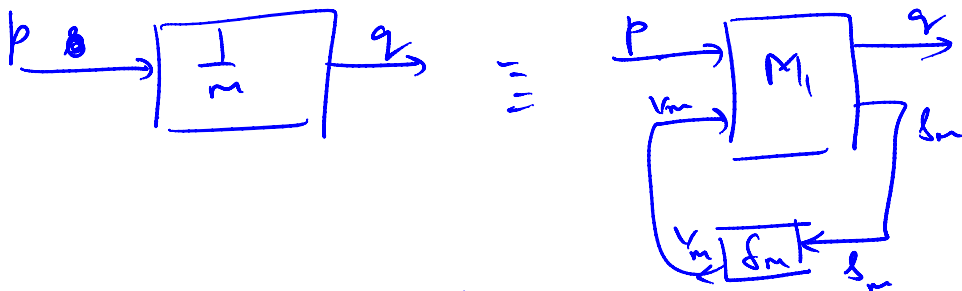
$$k = \bar{k}(1 + 0.1\delta_k)$$

$$c = \bar{c}(1 + 0.1\delta_c)$$

$$\frac{1}{m} = \frac{1}{\bar{m}(1 + 0.1\delta_m)}$$

$$\frac{1}{\bar{m}(1 + 0.1\delta_m)} \equiv F_e(M_1, \delta_m) \text{ where}$$

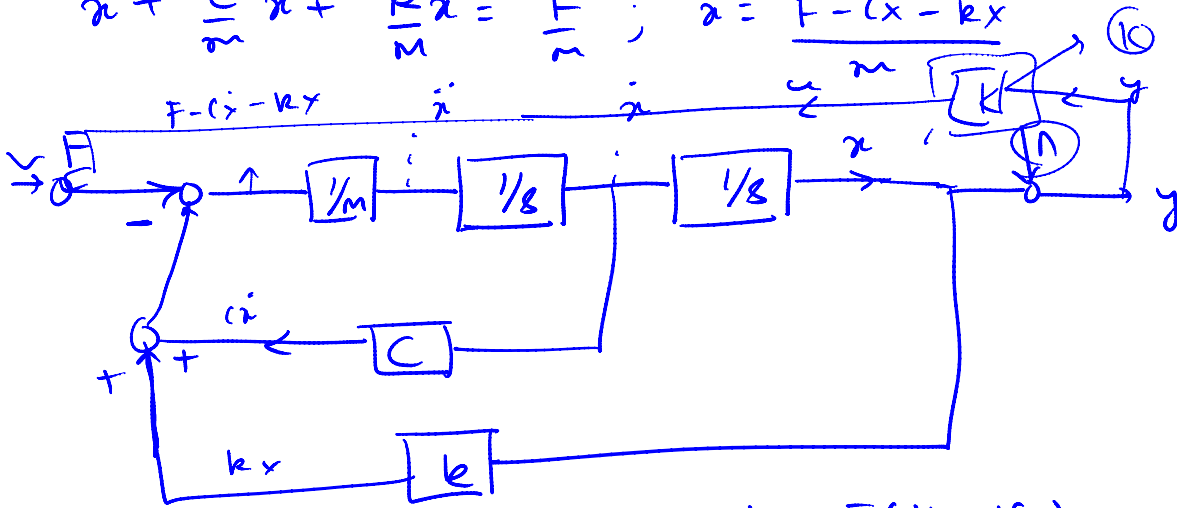
$$M_1 \equiv \begin{bmatrix} \frac{1}{\bar{m}} & -\frac{0.1}{\bar{m}} \\ 1 & -0.1 \end{bmatrix}$$



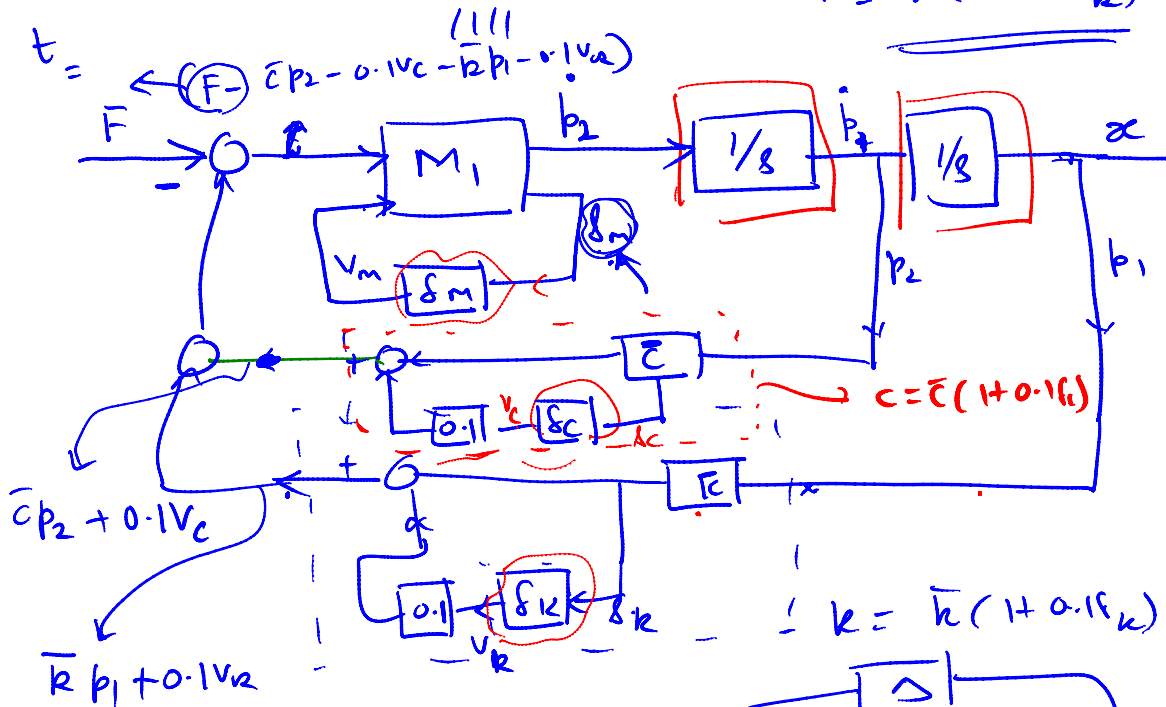
$$\begin{pmatrix} q \\ \delta_m \end{pmatrix} = \begin{bmatrix} \frac{1}{\bar{m}} & -\frac{0.1}{\bar{m}} \\ 1 & -0.1 \end{bmatrix} \begin{pmatrix} p \\ v_m \end{pmatrix}$$

$$\Rightarrow \begin{aligned} q &= \frac{1}{\bar{m}} p - \frac{0.1}{\bar{m}} v_m \\ \delta_m &= p - 0.1 v_m. \end{aligned}$$

$$\ddot{x} + \frac{c}{m} \dot{x} + \frac{k}{m} x = \frac{F}{m}; \quad \ddot{x} = \frac{F - c\dot{x} - kx}{m}$$



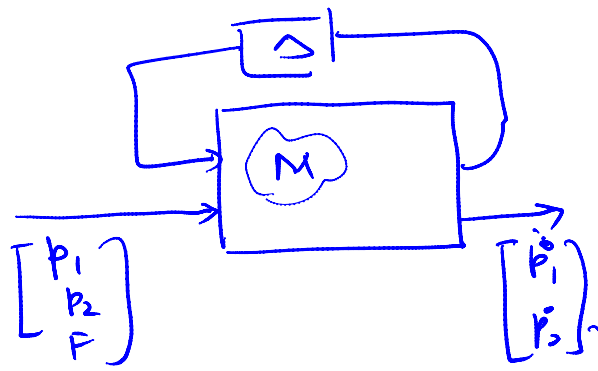
$$k = \bar{k}(1 + 0.1\delta_k)$$



$$k = \bar{k}(1 + 0.1\delta_k)$$

$$p_1 \equiv \dot{x}$$

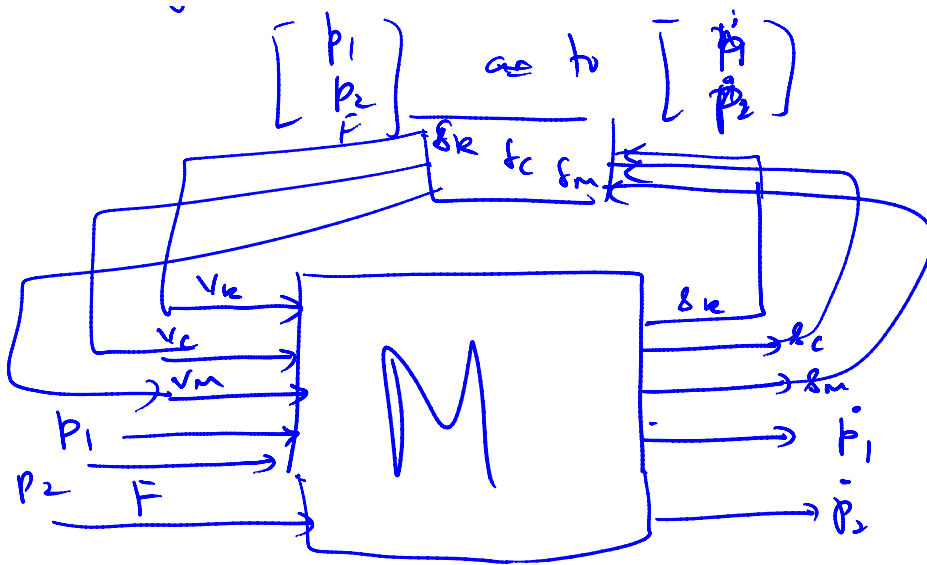
$$p_2 \equiv x$$



Find M such that

$$F_u(M, \Delta) \text{ with } \Delta = \begin{bmatrix} \delta_k & 0 & 0 \\ 0 & \delta_c & 0 \\ 0 & 0 & \delta_m \end{bmatrix}$$

gives the map from $\begin{bmatrix} p_1 \\ p_2 \end{bmatrix}$ to $\begin{bmatrix} \dot{p}_1 \\ \dot{p}_2 \end{bmatrix}$

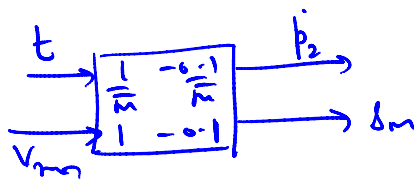


$$\delta_k = [0 \ 0 \ 0 \ \bar{k} \ 0 \ 0]$$

$$\delta_c = [0 \ 0 \ 0 \ 0 \ \bar{c} \ 0]$$

$$\delta_m = [$$

$$\begin{bmatrix} v_k \\ v_c \\ v_m \\ p_1 \\ p_2 \\ F \end{bmatrix}$$



$$\begin{bmatrix} p_2 \\ \delta_m \end{bmatrix} = \begin{bmatrix} \frac{1}{m} & -0.1 \\ 1 & -0.1 \end{bmatrix} \begin{bmatrix} t \\ v_m \end{bmatrix}$$

$$p_2 = \frac{1}{m} t - 0.1 v_m$$

$$\delta_m = t - 0.1 v_m$$

$$= F - \bar{c} p_2 - 0.1 v_c - \bar{k} p_1 - 0.1 v_k$$

$$= F - \bar{c} p_2 - 0.1 v_c - \bar{k} p_1 - 0.1 v_k - 0.1 v_m$$

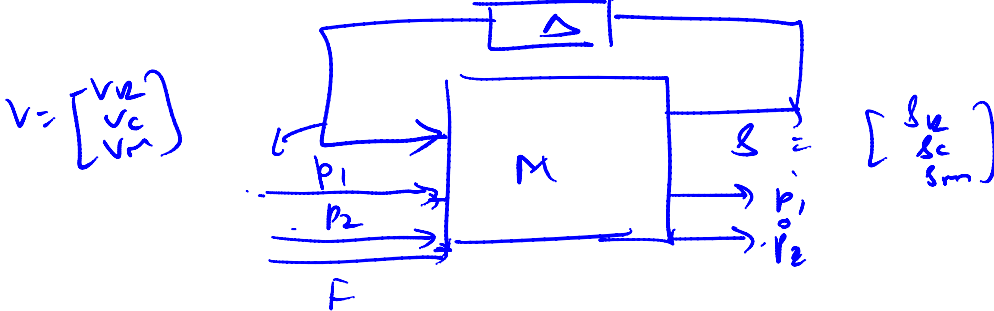
$$\delta_m = [0.1 \ -0.1 \ -0.1 \ -\bar{k} \ -\bar{c} \ 1] \begin{bmatrix} v_k \\ v_c \\ v_m \\ p_1 \\ p_2 \\ F \end{bmatrix}$$

$$\dot{p}_1 = p_2 = \begin{bmatrix} 0 & 0 & 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} p_1 \\ p_2 \\ F \\ v_k \\ v_c \\ v_m \\ p_1 \\ p_2 \\ F \end{bmatrix}$$

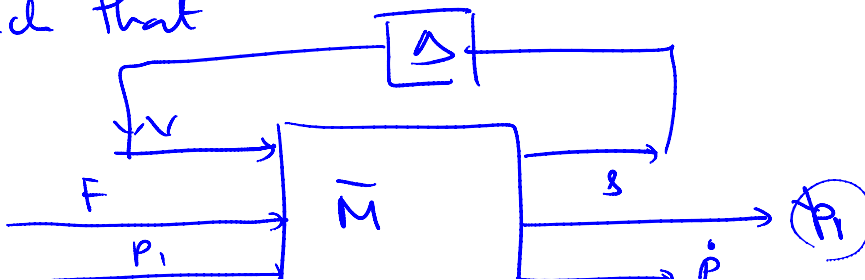
$$\dot{p}_2 = \frac{F - (p_2 - 0 \cdot v_c - k p_1 - 0 \cdot v_a)}{M} - 0 \cdot \frac{v_m}{M}$$

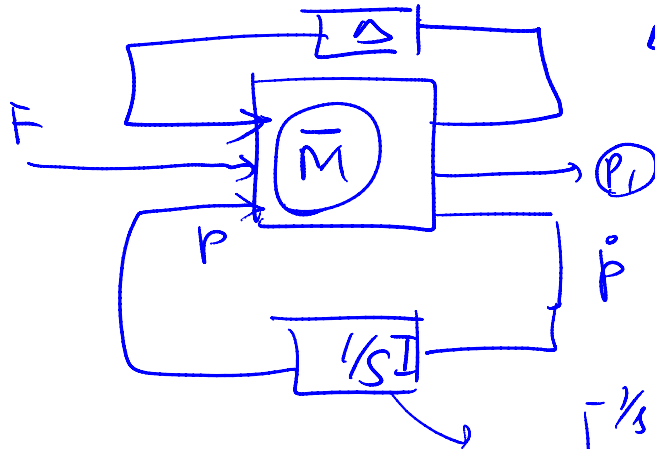
$$= \begin{bmatrix} -0 \cdot \frac{1}{M} & -\frac{1}{M} & -\frac{1}{M} & 0 & \frac{1}{M} & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} v_k \\ v_c \\ v_m \\ p_1 \\ p_2 \\ F \end{bmatrix}$$

$$\begin{bmatrix} \delta_k \\ \delta_c \\ \delta_m \\ p_1 \\ p_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 & k & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ -0 \cdot \frac{1}{M} & -\frac{1}{M} & -\frac{1}{M} & 0 & 0 & 1 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ -\frac{1}{M} & 0 & 0 & 0 & 0 & 0 \\ -\frac{1}{M} & 0 & 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} v_k \\ v_c \\ v_m \\ p_1 \\ p_2 \\ F \end{bmatrix} \rightarrow \begin{matrix} \delta_k \\ \delta_c \\ \delta_m \\ p_1 \\ p_2 \end{matrix}$$



Let's assume that \bar{M} is determined such that





$$D = \begin{bmatrix} f_k & 0 \\ 0 & f_c & f_m \end{bmatrix}$$

with $|f_k| \ll 1$
 $|f_c| \ll 1$
 $|f_m| \ll 1$

$$\begin{bmatrix} -1/s & 0 \\ 0 & 1/s \end{bmatrix} = \frac{1}{s} I$$

$$p \rightarrow \left\{ F_u \quad (F_e(\bar{M}, \frac{1}{s}I), \Delta) \right\} F$$

$$u = K_y + \underset{\uparrow}{V} \quad \text{where} \quad y = p_1 + n$$